Improved first generation current conveyor based on self-cascode current mirror

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Abstract — This paper presents an improved first generation current conveyor. The proposed circuit is based on a CMOS translinear loop and self-cascode current mirrors. The structure of the circuit is analyzed and compared with a classical CCI structure. PSpice simulation results for the proposed circuit in 0.35 μm CMOS technology are given to verify the theoretical analysis.

Keywords — current conveyor, self-cascode mirror, CMOS.

I. INTRODUCTION

Since Sedra published first generation current conveyor (CCI) (1968), current conveyor based circuits have received lots of attention in analog signal processing applications, such as filter [1] function generator [2], impedance function synthesis [3], etc. [4]. CCs are unity-gain amplifiers widely used by analog designers, in particular because they offer a number of advantages, such as better linearity, wider bandwidth, and design flexibility over conventional voltage-mode active devices.

Several types of CC exist covering first, second (CCII) and third generation (CCIII). Whilst CCII is considered the most versatile and used CC, the first generation CCI is well known for its simplicity.

\[
\begin{align*}
I_Y & = 0 \\
V_X & = 1 \\
I_Z & = 0 \pm 1
\end{align*}
\]

The definition matrix (1) along with input-output equations (2) and nodes impedance level (Table 1) presents the main characteristics of the ideal CCI (CCI+ and CCI-).

\[
\begin{align*}
I_Y &= \pm I_Z = I_x \\
V_X &= V_Y
\end{align*}
\]

The CCI symbol and CMOS structure are given in Fig. 1 and Fig. 2.

A good CCI structure must provide several features:

- Very low input impedance, very high Y and Z impedances, unity voltage and current gains between ports, large dynamic input and output current and voltage ranges.

![Fig. 1. CCI symbol](image1)

![Fig. 2. Typical CMOS CCI+ structure](image2)

II. IMPROVED SELF-CASCODE CCI

A. Simple current mirror based CCI structure

The typical CMOS structure (Fig.2) is a class AB current conveyor that offers the advantages of high dynamic range, wide bandwidth and non-slew rate limited performance. Due to the low quality of the simple current mirror (CM) this CCI structure assures moderate performances in respect of input/output impedance.

Equations for input and output resistances for CCI in Fig.2 are given in (3), (4) and (5).

\[
R_X \equiv \left( \frac{g_{ds2} + g_{ds4}}{g_{m2}g_{m4}} + \frac{g_{ds1} + g_{ds3}}{g_{m1}g_{m2}} \right)
\]

\[
R_Y \equiv \frac{g_{ds7} + g_{ds8}}{g_{m7}g_{m8}}
\]

\[
R_Z \equiv \frac{g_{ds6} + g_{ds9}}{g_{m6}g_{m8}}
\]

To decrease the input resistance on port X, \( R_X \) and increase input resistance on port Y, \( R_Y \), and output resistance on port Z, \( R_Z \), the designer must increase the CMI output resistance. An efficiently improvement cannot

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be obtained due to CMs structure. This limitation imposes to replace simple CM with better current mirrors.

B. Cascode mirror based CCI structure

Several papers present AB class current conveyors using improved current mirrors: cascode mirror [5], high-swing mirror [6], low voltage self-cascode [7], etc. Fig. 3 shows a CCI based on cascode current mirror (CCM).

![Fig. 3. Cascode mirror based CCI structure](image)

This current mirror structure provides much greater output resistance (6) and thus CCI input and output resistances are improved.

\[ r_o = r_{o3a} \left( \frac{g_m r_{o3}}{1 + g_m r_{o3}} \right) \] (6)

CCM requires minimum input (7) and output voltage (8) larger than CM to keep all transistors in saturation.

\[ V_{\text{output,min}} = V_{th3} + 2 \times V_{DSat} \] (7)

\[ V_{\text{input,min}} = 2 \times (V_{th3} + V_{DSat}3,4) \] (8)

Using CMs instead of CMs in CCI dramatically reduce input and output voltage dynamic ranges. This is a disadvantage than cannot be accepted for circuits that use low voltage power supply.

Replacing CCM with high-swing current mirror is out of purpose of this paper because requires additional bias circuitry that increases CCI complexity.

C. Self cascode mirror based CCI structure

The purpose of this paper is to propose and analyze a new AB class CCI structure based on self-cascode mirrors (SCCM). The proposed circuit is given in Fig. 4 and based on 6 SCCMs [8]. This structure maintains CCI circuit complexity as low as possible but provides good performance in terms of input and output resistances and voltage dynamic range.

![Fig. 4. New self-cascode CCI+](image)

A well-designed SCCM must assure that all transistors work in saturation. Reference [8] shows a condition (9) to keep transistors T3A and T4A in saturation. This is easy to fulfill in a multi-threshold CMOS process.

\[ V_{th4A} - V_{th4} \geq V_{DSat4} \] (9)

In a standard CMOS technology this condition can be accomplish using SCE (short-channel effect) and (10) [9].

\[ \frac{\beta_{4A}}{\beta_4} \leq \left( \frac{n-1}{n} + \frac{V_{th4A} - V_{th4}}{V_{GS4A} - V_{th4A}} \right)^2 \] (10)

n – slope factor (about 1.3), \( \beta = \mu C_0 W/L \).

Reference [10] presents a methodology based on SCE and RSCE (reverse short-channel effect) [11] useful to design both pMOS and nMOS SCCMs.

This kind of current mirror shows an output resistance similar to that of the cascode mirror but input and output voltage close to the simple CM. Table 2 gives a comparative view for output impedance, input and output voltage for the three current mirrors previous presented. It is obvious that SCCM is better than CM and equal with CCM regarding output resistance. SCCM demands a minimum input voltage similar with CM but much less than CCM. Minimum output voltage required by SCCM is less that similar voltage for CCM and very close to CM once. This SCCM shows improved output resistance without affecting voltage dynamic ranges.

Input and output resistances for CCI in Fig. 4:

\[ R_x = \frac{g_{m2} g_{m4} + g_{m2} g_{m8} + g_{m2} g_{m4} g_{m8}}{g_{m2} g_{m4} g_{m8}} \]

(11)
TABLE 2: CM, CCM AND SCCM MAINLY CHARACTERISTICS

<table>
<thead>
<tr>
<th></th>
<th>Current mirror CM</th>
<th>Cascode current mirror CCM</th>
<th>Self cascade current mirror SCCM</th>
</tr>
</thead>
<tbody>
<tr>
<td>Output resistance</td>
<td>( r_o = r_{o3} )</td>
<td>( r_o = r_{o3,4}(g_{m3}r_{o3}) )</td>
<td>( r_o = r_{o3,4}(g_{m3}r_{o3}) )</td>
</tr>
<tr>
<td>Minimum output voltage</td>
<td>( V_{DSsat3A} )</td>
<td>( V_{th3} + 2*V_{DSsat} )</td>
<td>( V_{th3} - V_{th3A} + V_{DSsat} )</td>
</tr>
<tr>
<td>Minimum input voltage</td>
<td>( V_{th3} + V_{DSsat3} )</td>
<td>( 2*(V_{th3} + V_{DSsat3A}) )</td>
<td>( V_{th3} + V_{DSsat4A} )</td>
</tr>
</tbody>
</table>

\[
R_Y \cong \frac{g_{m3}}{g_{ds3}r_{o3}A} \quad (12)
\]

\[
R_Z \cong \frac{g_{mV_i}r_{onA}}{g_{mp}r_{onA}A} \quad (13)
\]

Equations (11), (12) and (13) show that new CCI structure achieves greater resistances on ports \( Y \) and \( Z \) and smaller resistance on port \( X \).

Fig. 5 shows CCI- structure based on self cascade current mirror.

III. DESIGN CIRCUITS

Both circuits from Fig. 2 and Fig. 4 were designed in a standard 0.35 \( \mu m \) CMOS technology. All the transistors in Fig. 4 were designed to work in saturation mode using (10) and SCE for sizing nMOS and RSCE for sizing pMOS [10]. Table 3 and Table 4 show \( W \) and \( L \) sizes for transistors in Fig. 2 and Fig. 4.

TABLE 3: \( W \) AND \( L \) SIZES FOR SELF-CASCODE CCI+

<table>
<thead>
<tr>
<th>( CCI^+ ) new</th>
<th>( W[\mu m] )</th>
<th>( L[\mu m] )</th>
</tr>
</thead>
<tbody>
<tr>
<td>( T_1, T_2 )</td>
<td>26</td>
<td>3.3</td>
</tr>
<tr>
<td>( T_3, T_4, T_S )</td>
<td>68.4</td>
<td>1</td>
</tr>
<tr>
<td>( T_{3A}, T_{4A}, T_{NA} )</td>
<td>3.8</td>
<td>0.65</td>
</tr>
<tr>
<td>( T_5, T_6 )</td>
<td>10.2</td>
<td>2.8</td>
</tr>
<tr>
<td>( T_7, T_8, T_P )</td>
<td>96</td>
<td>0.55</td>
</tr>
<tr>
<td>( T_{7A}, T_{8A}, T_{PA} )</td>
<td>32</td>
<td>3.4</td>
</tr>
</tbody>
</table>

TABLE 4: \( W \) AND \( L \) SIZES FOR TYPICAL CCI+

<table>
<thead>
<tr>
<th>( CCI^+ ) typical</th>
<th>( W[\mu m] )</th>
<th>( L[\mu m] )</th>
</tr>
</thead>
<tbody>
<tr>
<td>all nMOS</td>
<td>15</td>
<td>2.5</td>
</tr>
<tr>
<td>all pMOS</td>
<td>55.5</td>
<td>2.5</td>
</tr>
</tbody>
</table>

IV. SIMULATION RESULTS

The circuit was simulated using PSpice. Using power supplies of \( \pm 2.5V \) and the sizes in Table 3 and Table 4 self-bias currents are 110\( \mu A \) for Fig. 2 and 55\( \mu A \) for Fig. 4. Table 5 shows the input and output impedances, voltage and current gains, bias currents and active areas for the proposed CCI+ and for a typical CCI+. For almost the same active area the new CCI provides the same input resistance on port \( X \) but the bias current is halved. There are good improvements in respect of input impedance on port \( Y – 13.5 \) times and output impedance on port \( Z – 8 \) times. Current gains \( \beta \) and \( \gamma \) errors are reduced from 0.7% to 0.11%. Voltage gain \( \alpha \) is reduced from 0.72% to 0.38%.

TABLE 5: NEW \( CCI^+ \) VERSUS TYPICAL \( CCI^+ \) PERFORMANCEs

<table>
<thead>
<tr>
<th>( CCI^+ ) new</th>
<th>( CCI^+ ) Typical</th>
</tr>
</thead>
<tbody>
<tr>
<td>Technology</td>
<td>CMOS 0.35( \mu m ), ( \pm 2.5V )</td>
</tr>
<tr>
<td>Active area</td>
<td>926 ( \mu m^2 )</td>
</tr>
<tr>
<td>Bias current</td>
<td>55 ( \mu A )</td>
</tr>
<tr>
<td>( R_x )</td>
<td>20.02 ( \Omega )</td>
</tr>
<tr>
<td>( R_y )</td>
<td>6.86 ( M\Omega )</td>
</tr>
<tr>
<td>( R_z )</td>
<td>10.89 ( M\Omega )</td>
</tr>
<tr>
<td>( V_x/V_y(%)  )</td>
<td>0.9962</td>
</tr>
<tr>
<td>( I_{d}/I_{c}(%) )</td>
<td>1.0011</td>
</tr>
<tr>
<td>( I_{d}/I_{c}(%) )</td>
<td>0.9989</td>
</tr>
<tr>
<td>( C_Y )</td>
<td>105 ( \text{fF} )</td>
</tr>
<tr>
<td>( C_Z )</td>
<td>85 ( \text{fF} )</td>
</tr>
</tbody>
</table>

Fig. 6 shows input and output impedances for both the new \( CCI^+ \) and a typical \( CCI^+ \).

Fig. 7 presents the voltage tracking error between \( Y \) and \( X \) ports. It can be seen that the input voltage range is almost the same for the new CCI based on SCCM as for the typical CCI based on CM.
To demonstrate the usefulness of the improved features for the CCI next are presented two applications for this circuit – negative impedance convertor (NIC) and negative admittance/impedance convertor (NAIC). Fig. 8 and Fig. 9 show these circuits.

NIC input impedance is given by (14) and NAIC input impedance is given by (15)

\[
Z_{i1} = \frac{V_i}{I_X} = \frac{V_Y}{I_Y} = -Z_i \quad (14)
\]

\[
Z_{i2} = \frac{V_i}{I_i} = -\frac{1}{Z_2}R_1R_2 = -Y_2R_1R_2 \quad (15)
\]

Both circuits were simulated with typical CCI and new CCI. Fig. 10 shows simulation results. \(Z_1\) and \(Z_2\) are capacitors with value 10pF and resistors have equal values, \(R_1=R_2=100\,\Omega\). For circuits designed using CCI based on SCCM input impedances have extended frequency ranges where close approximate an ideal behavior. Frequency ranges are extended with more than 1.5 decades towards lower frequency. This improvement is consequence of higher input and output resistance on ports \(Y\) and \(Z\) for new first generation current conveyor.

V. CONCLUSION

This paper has presented a novel CCI structure based on self-cascode current mirror. The results show that the proposed circuit improves performances in respect of input/output impedances and voltage/current gains maintaining large dynamic voltage ranges.

REFERENCES


